

# CFD Based Air Flow and Contamination Modeling of Subway Stations

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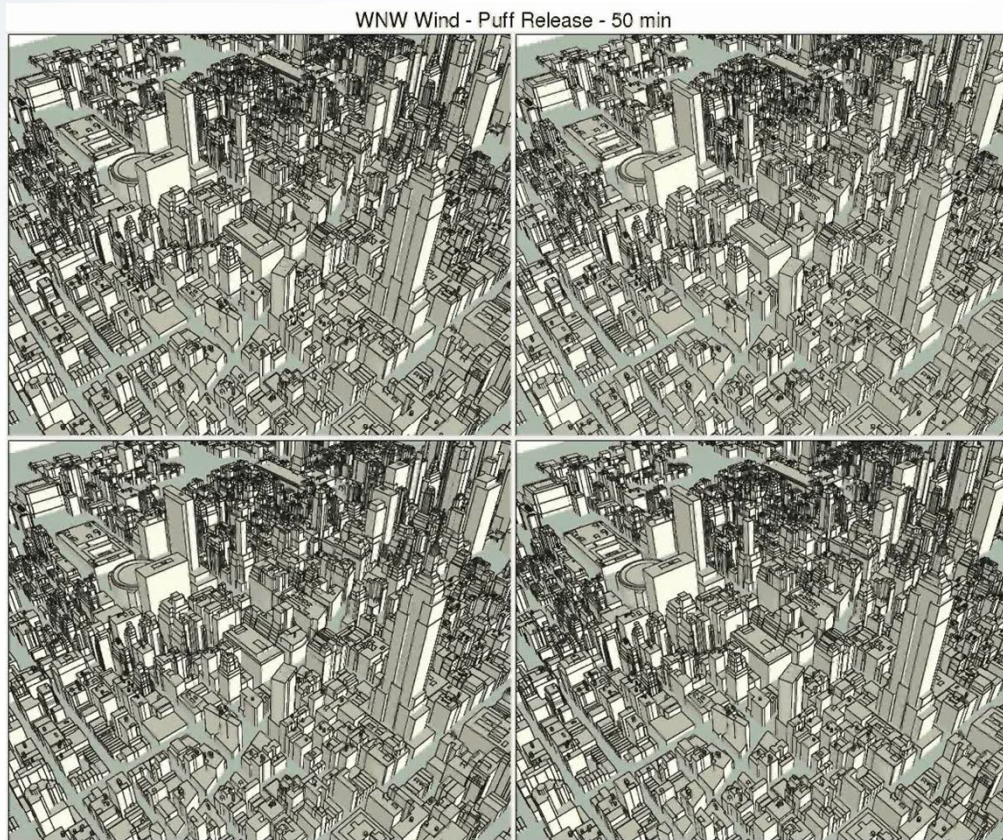
Center for Computational Fluid Dynamics,  
George Mason University



# Urban Flows

- Computational fluid dynamic simulations play an important role in predicting atmospheric mixing, transport and dispersion in urban environments.

**4 iso-surfaces of contaminant concentration during a release in Manhattan**



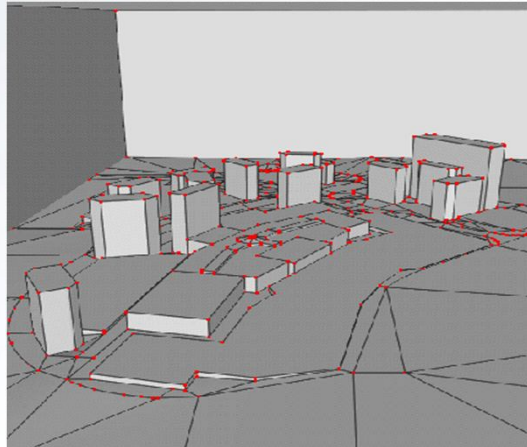


# Computational Pipeline

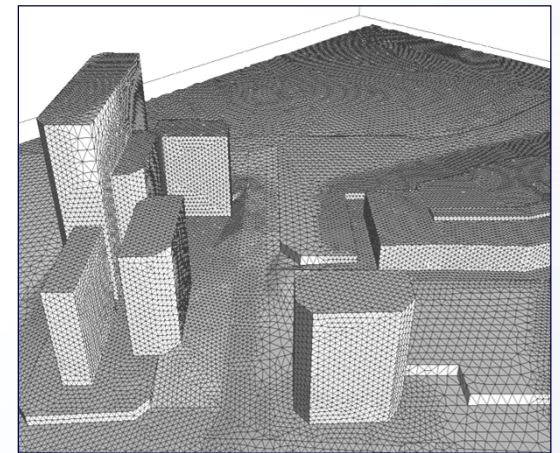
**Site Survey**



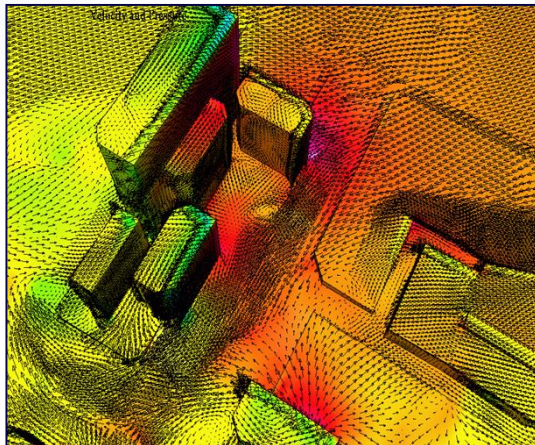
**Geometric Modeling**



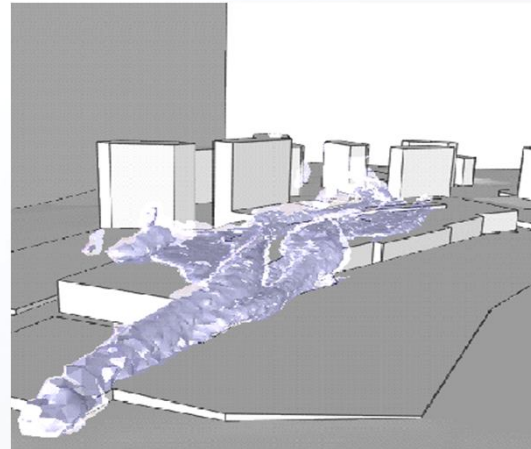
**Unstructured Meshing**



**Flow/Dispersion Solver**



**Post-processing**



# CFD Based Air Flow Modelling

- Subway stations are important urban infrastructures with complex spatiotemporal air flow patterns.
  - Use computational fluid dynamics to predict temperature, mixing, transport and dispersion.
  - Enable future improvements in safety and health.

**Sarin Attack**  
Tokyo, Japan, 1995



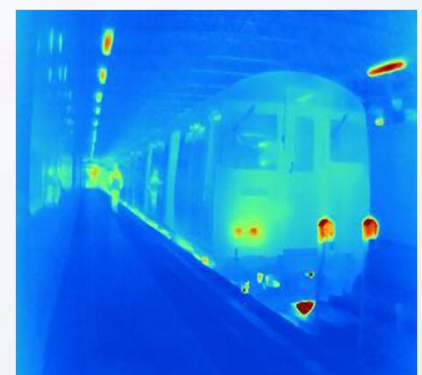
**Subway Fire**  
Daegu, Korea, 2003



**Air Quality Studies**  
Buenos Aires, AR, 2009



**Temperature Regulation**  
(future design tool)



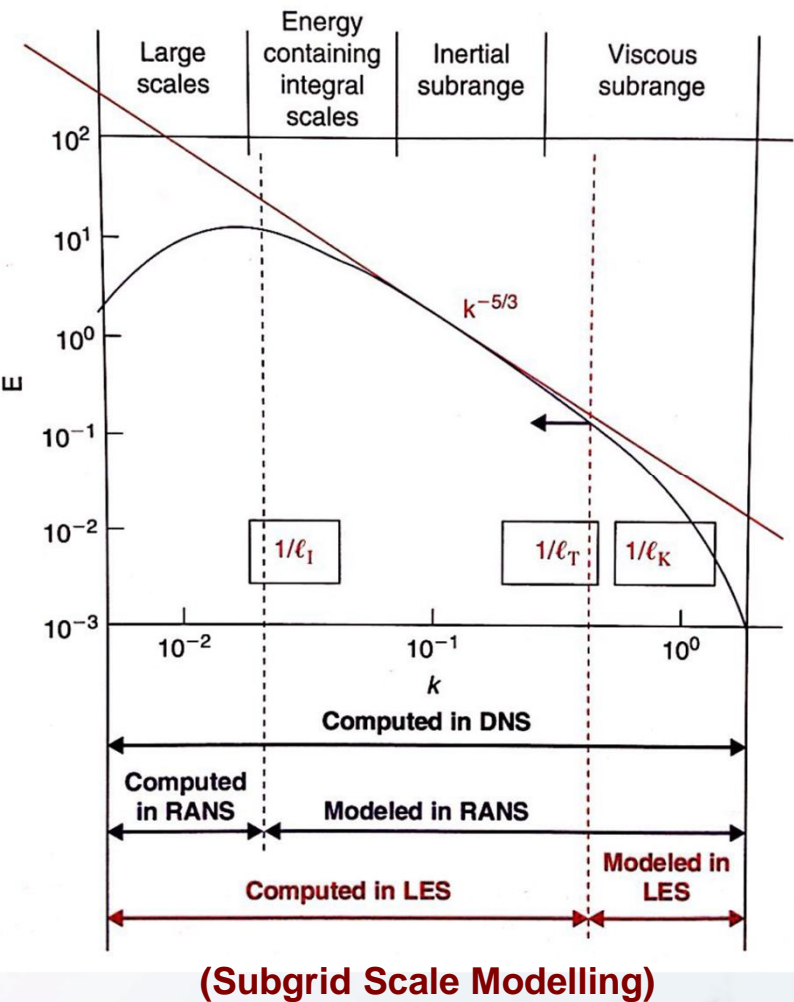
# Urban Flow Simulations

<b>Subway Environment Simulator</b> (American Public Transit Association)	<b>Fire Dynamics Simulator</b> (NIST)	<b>Air Quality Simulation</b> (Private & commercial codes)
<b>~1975</b>	<b>~2003</b>	<b>~2005</b>
<b>Continuity Equation</b>	<b>Navier-Stokes</b>	<b>Navier-Stokes</b>
<b>Solves sets of linear equations for bulk mean air flow (analogous to current in a Kirchhoff circuit)</b>	<b>Large-eddy simulation (LES) code for low-speed flows, with an emphasis on smoke and heat.</b>	<b>Dynamic inflow and outflow coupling to the street level. Realistic platform temperature distributions</b>
<b>Train motion modeled as a piston. Ignores nonlinear effects</b>	<b>Ignores effects of moving trains.</b>	<b>Piston driven flows. Experimental data available.</b>



# FEFLO Urban

- Explicit 2<sup>nd</sup> order time integrator
- 2<sup>nd</sup> order in space
- Large Eddy Simulation (LES) <sup>E</sup> for turbulence
- Smagorinsky (WALE) turbulence model
  - Wall Adapting Local Eddy Viscosity



# Time Discretization: $\Delta$ Scheme

- Advective / Diffusive Prediction:  $\vec{u}^n \rightarrow \vec{u}^*$

$$\left[ \frac{1}{\Delta t} - \theta \nabla \mu \nabla \right] (\vec{u}^* - \vec{u}^n) + \vec{u}^n \cdot \nabla \vec{u}^n + \nabla p = \nabla \mu \nabla \vec{u}^n$$

- Pressure Correction:  $p^n \rightarrow p^{n+1}$

$$\begin{aligned} \nabla \cdot \vec{u}^{n+1} &= 0, \quad \frac{\vec{u}^{n+1} - \vec{u}^*}{\Delta t} + \nabla(p^{n+1} - p^n) = 0 \\ \Rightarrow \nabla^2(p^{n+1} - p^n) &= \frac{\nabla \cdot \vec{u}^*}{\Delta t} \end{aligned}$$

- Velocity Correction:  $\vec{u}^* \rightarrow \vec{u}^{n+1}$

$$\vec{u}^{n+1} = \vec{u}^* - \Delta t \nabla(p^{n+1} - p^n)$$

# Previous Work: Piston Driven Flows

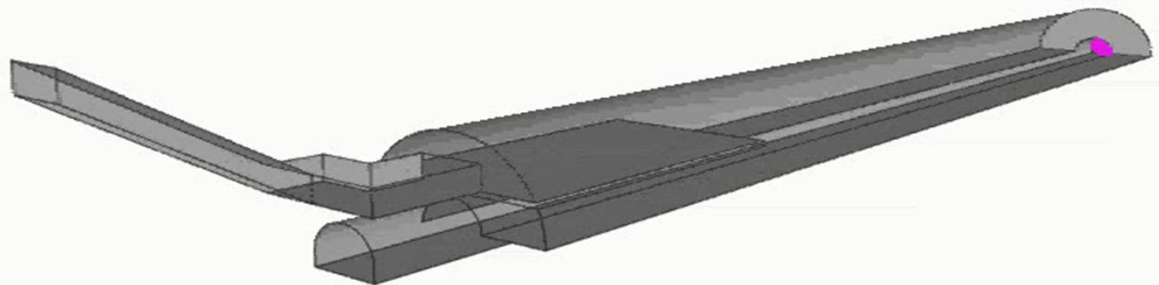
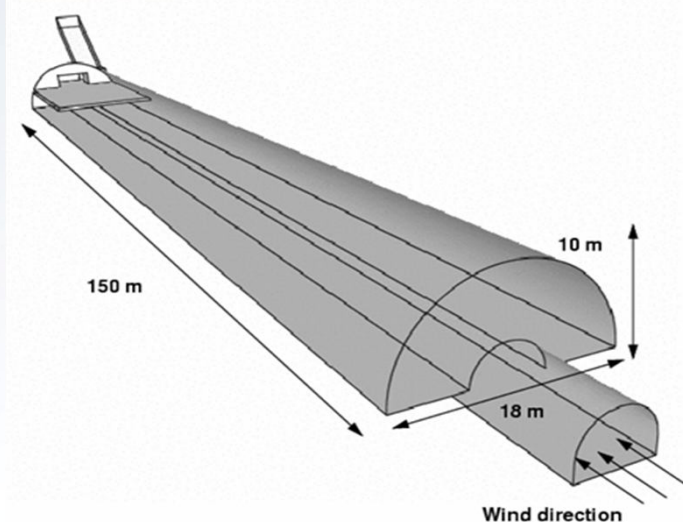
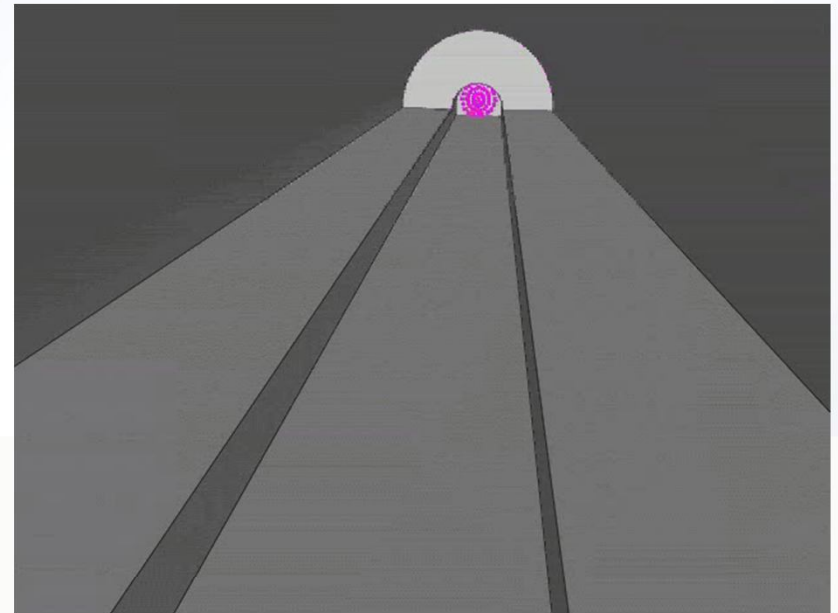
Conservation of mass

$$\nabla \cdot \vec{u} = 0$$

Conservation of momentum

$$\rho \left[ \frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u} \right] = \rho \vec{f}_e - \nabla p + \mu \nabla^2 \vec{u}$$

➤ Passive tracer release from tunnel





# Previous Work: Contaminant Release

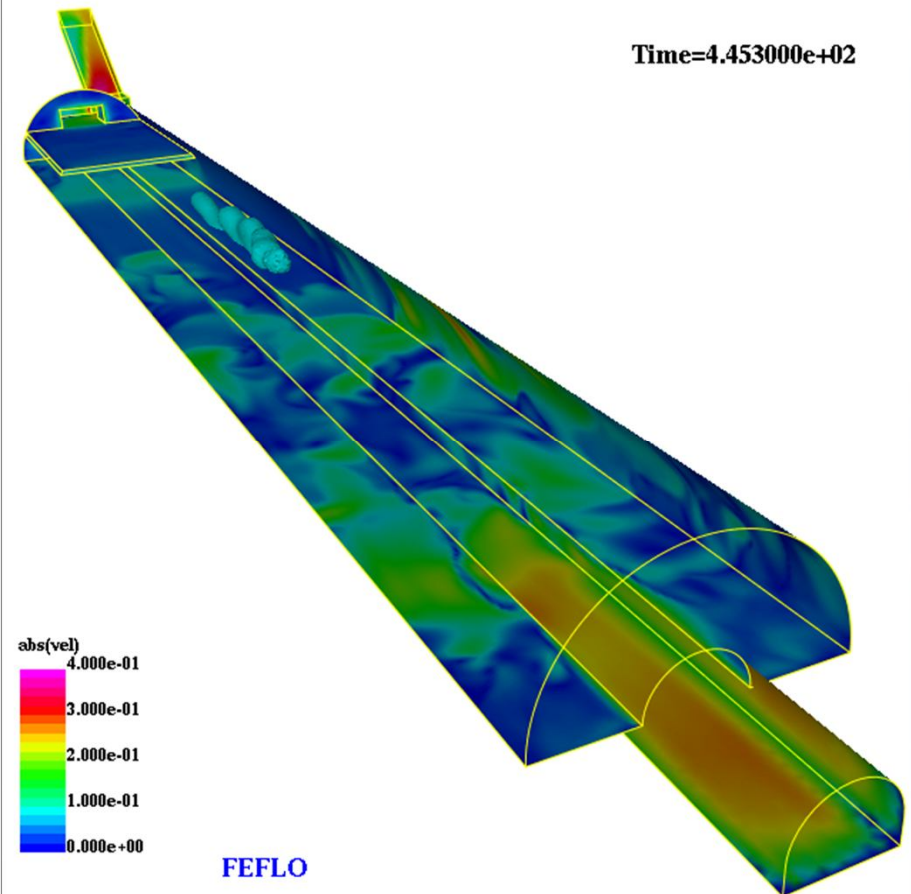
- Dispersion:

$$\frac{\partial c}{\partial t} + \vec{u} \cdot \nabla c = \nabla \cdot (D \nabla c) + S$$

- Dynamic Deactivation:  
Change in  $c$  only possible if

$$|\nabla c| > 0, \quad |S| > 0$$

- Algorithm: Every 5-10 Steps:
  - Identify Elements/Edges/Points Where Update Required
  - Surround Active Elements/Edges/Points With 'Safety Zone'
  - Only Compute/Update in Active Zone



# Objectives

## **Extend code to include dynamic components**

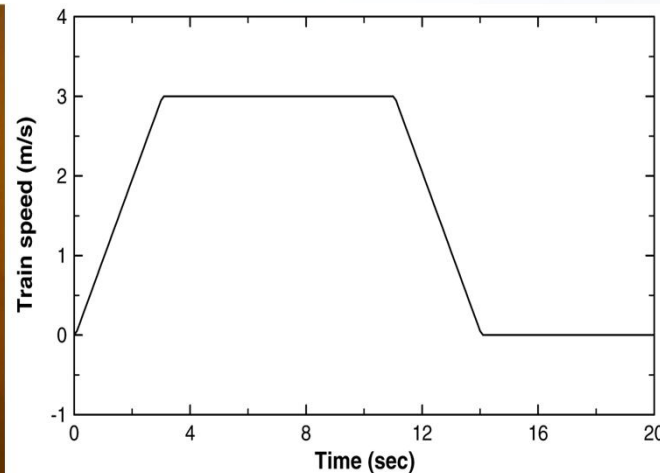
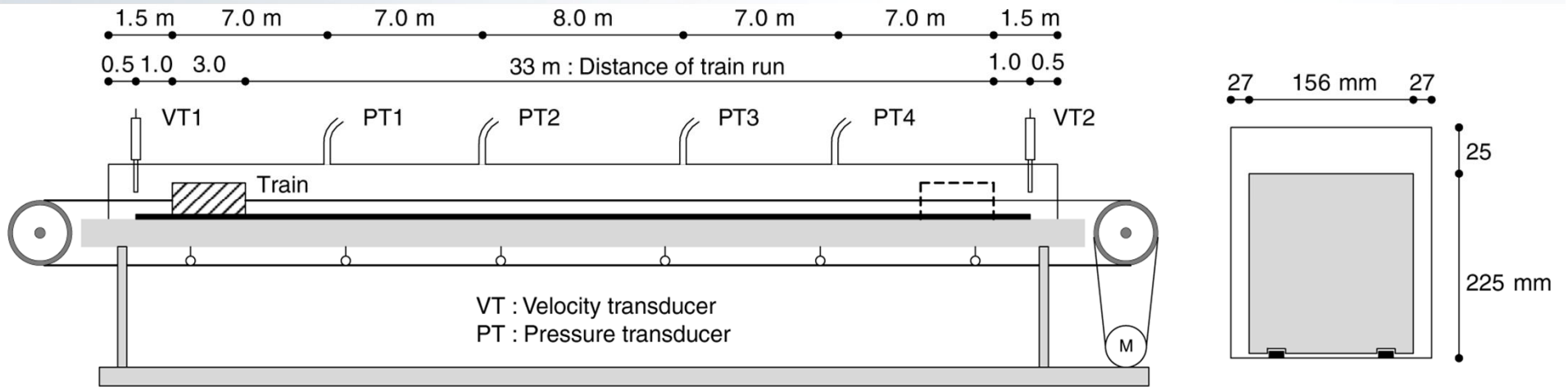
- Include train motion in CFD simulations
- Validate methodology against experimental data

## **Include detailed components**

- Multi-car trains with variable speeds and schedules
- Thermal effects
- Air flow coupling to the street level
- Realistic subway station geometries and networks
- Include sources of contamination
- Quantify the air flow dynamics in stations

# Kim and Kim's Experiment

Kim, J.Y., et. al. Experimental and numerical analyses of train-induced unsteady tunnel flow in subway.  
Tunneling and Underground Space Technology 22, 166-172. (2007)

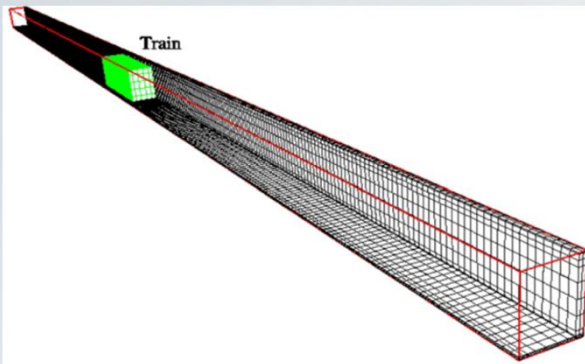


$$Re_{max} = 4.9 \times 10^4$$

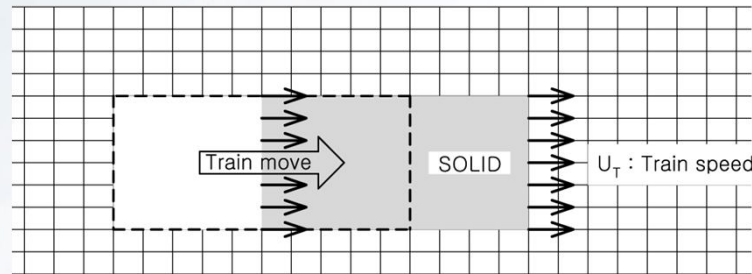
$$\Delta t_{sensor} = 0.1 s$$

$$U_{max} = 3.0 m/s$$

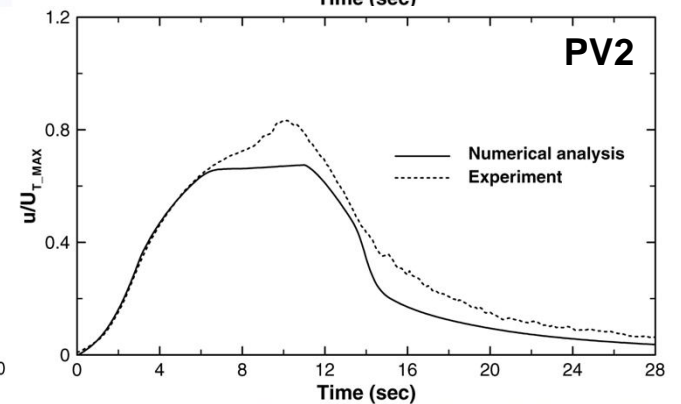
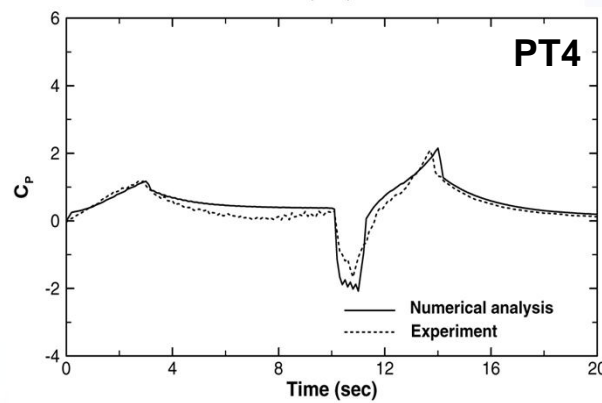
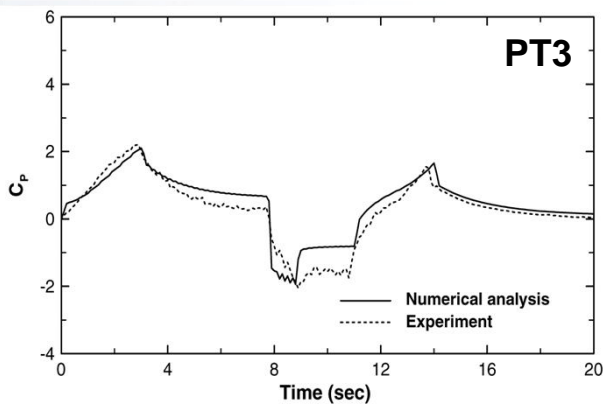
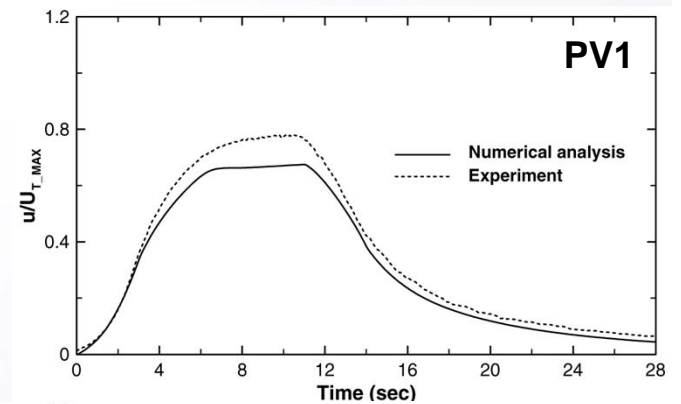
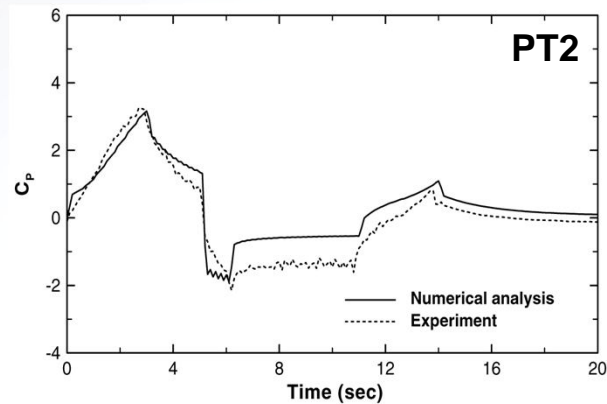
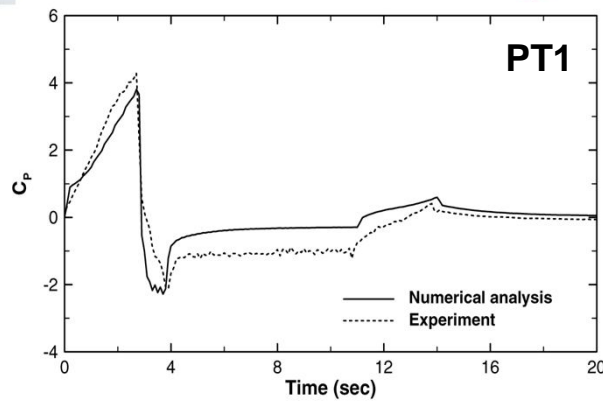
# Kim and Kim's Simulation



300k mesh cells



Spectral Solver  
Sharp front method

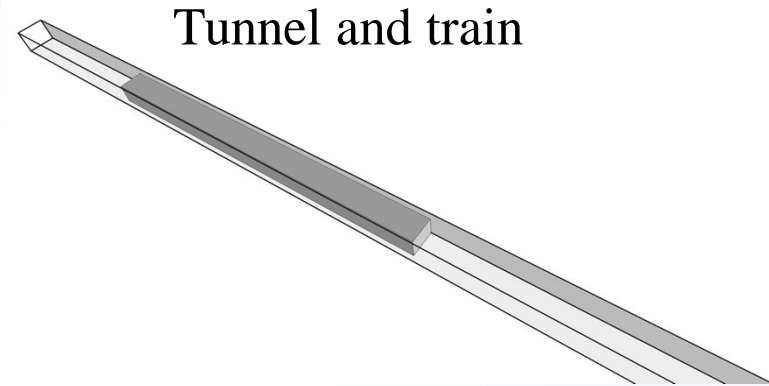
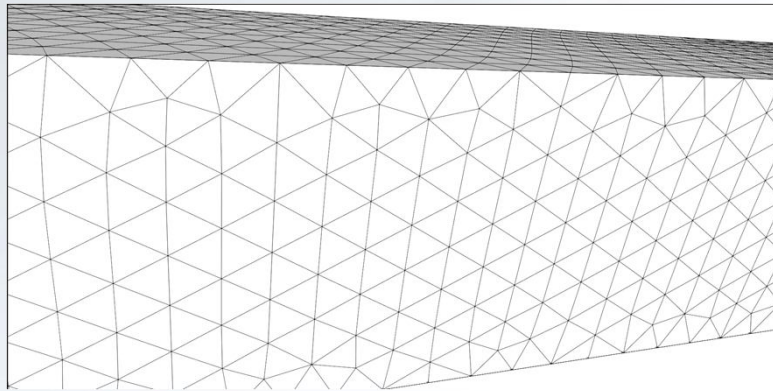




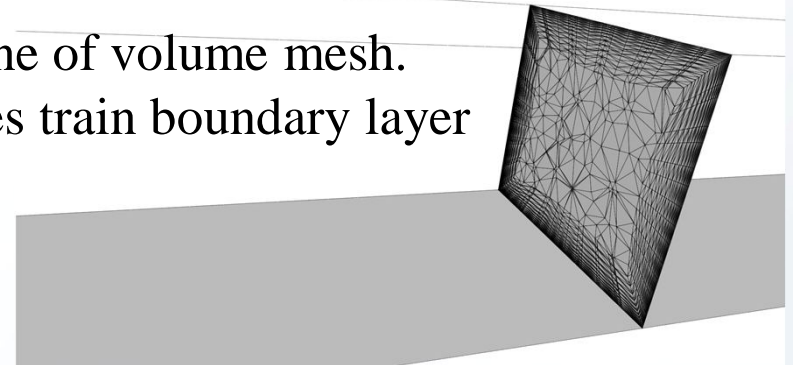
# How to Handle Dynamic Components?

Volume mesh: 4 M elements

Surface mesh

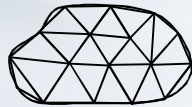


Cut plane of volume mesh.  
Resolves train boundary layer

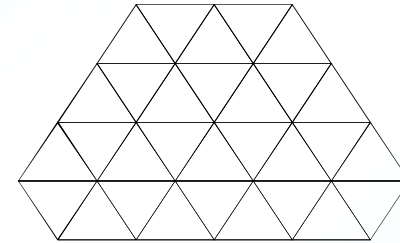


- Body fitted meshing
  - Requires local/global remeshing at each time step
- Immersed meshing
  - Represent the train as a volume tessellation and immerse it into a background mesh

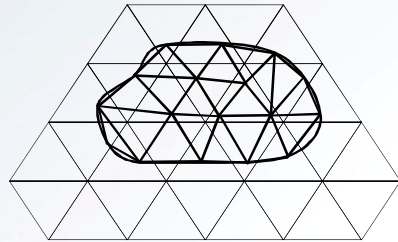
# Dynamic Meshing: Immersed Method



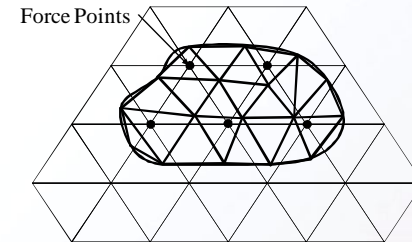
(a) Tessellated immersed body.



(b) Background or CFD mesh.



(c) CFD mesh and the immersed body.



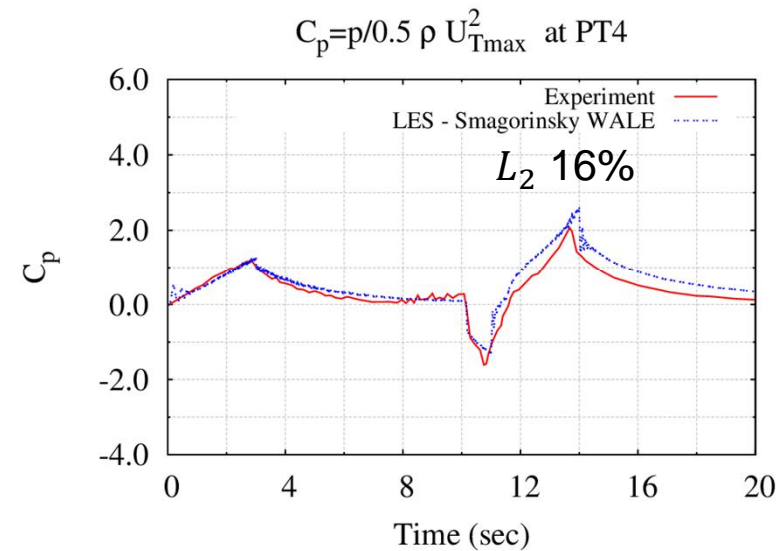
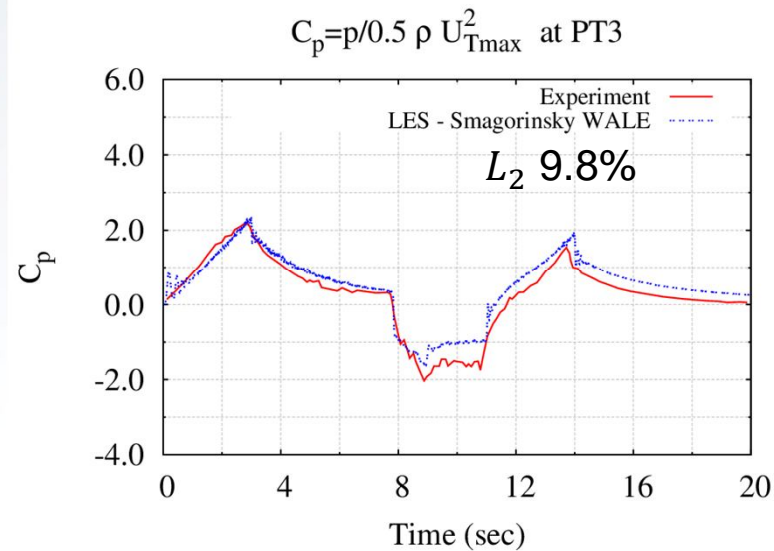
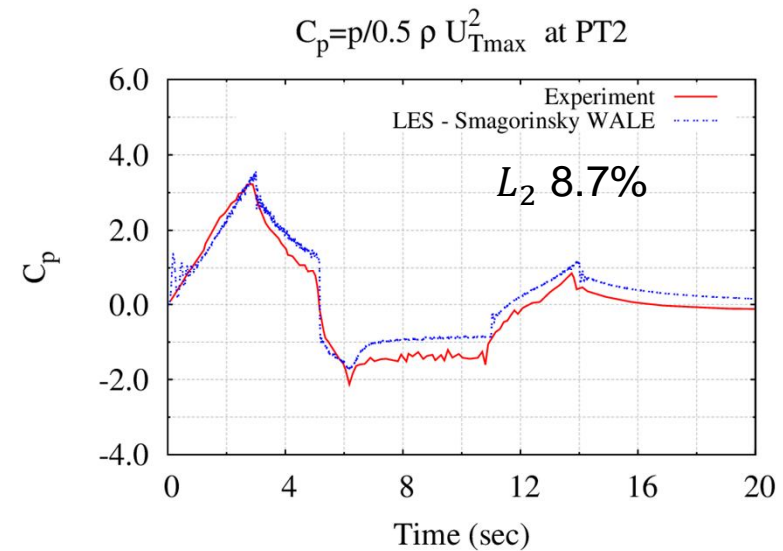
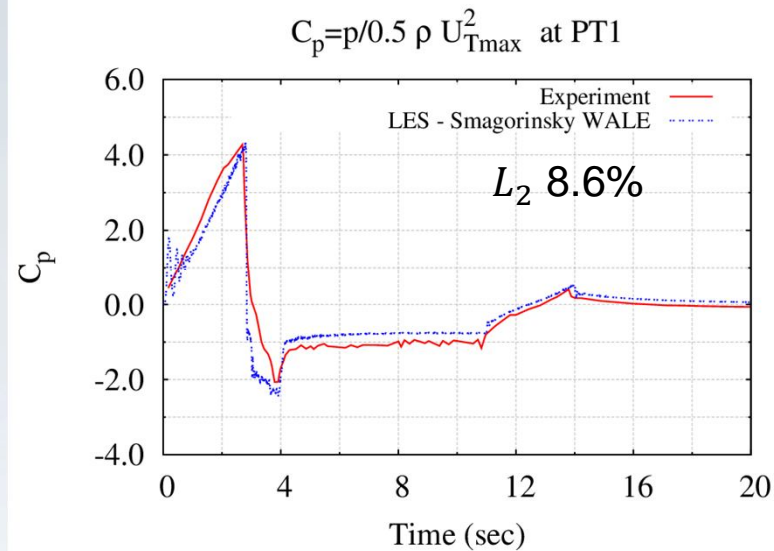
(d) Points in CFD mesh where forces are applied from immersed body.

$$\vec{f} = -c_0(\vec{w}_b - \vec{u}) \longrightarrow \text{Direct force scheme} \quad \mathbf{M} \frac{\Delta \vec{u}_i}{\Delta t} = \vec{r}_i + \vec{f}_i$$

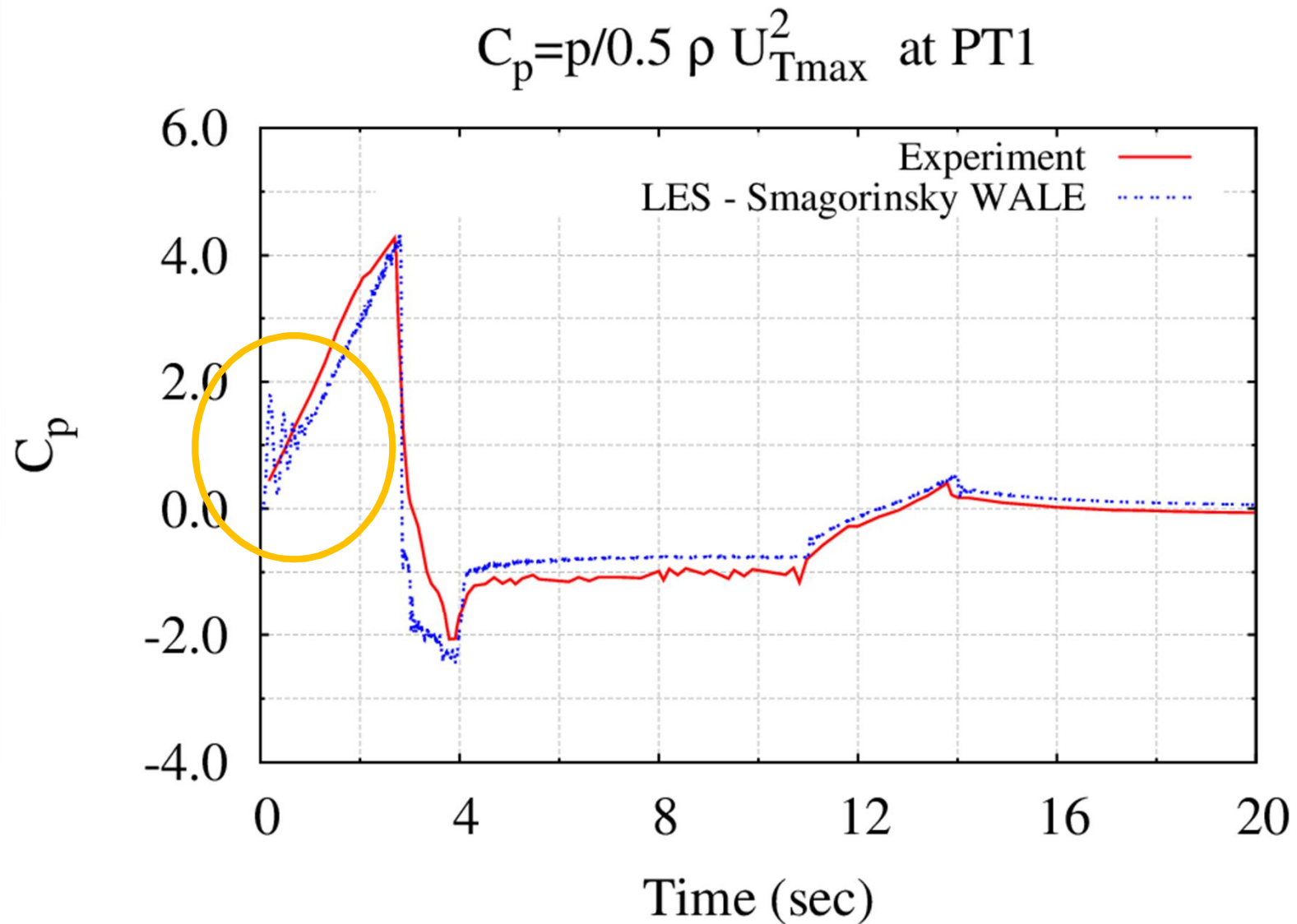
- $C_0$  small flow can't adjust rapidly enough to the motion of the body
- $C_0$  large produces artificial stiffness

$$\vec{f}_i = \mathbf{M} \frac{\vec{w}_i^{n+1} - \vec{u}_i^n}{\Delta t} - \vec{r}_i$$

# Pressure Comparison



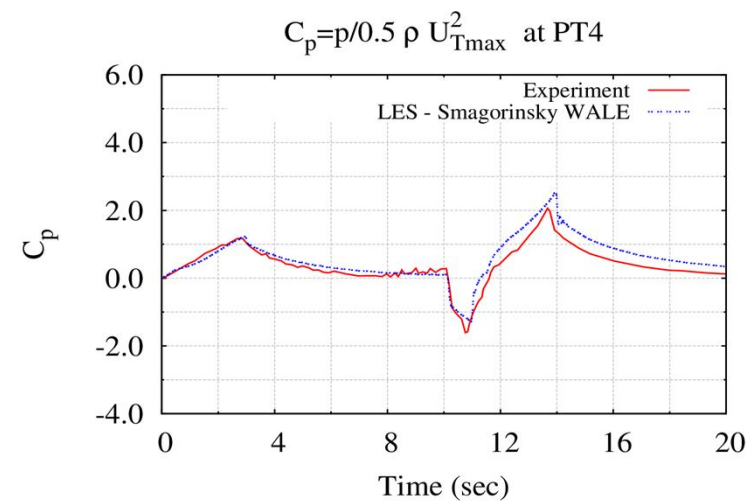
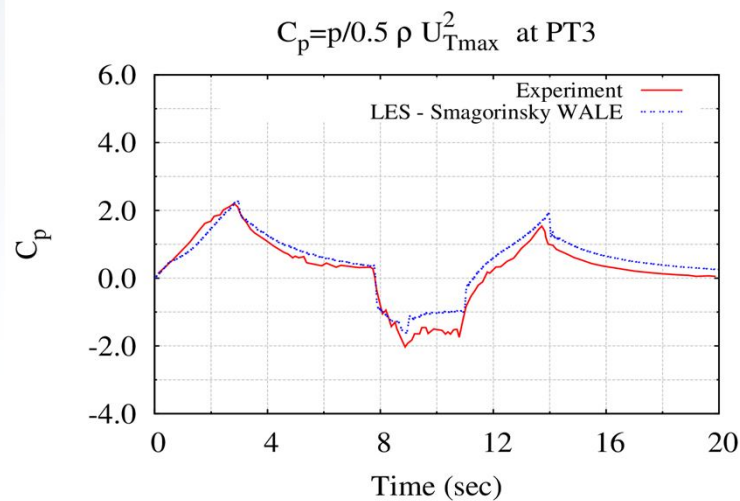
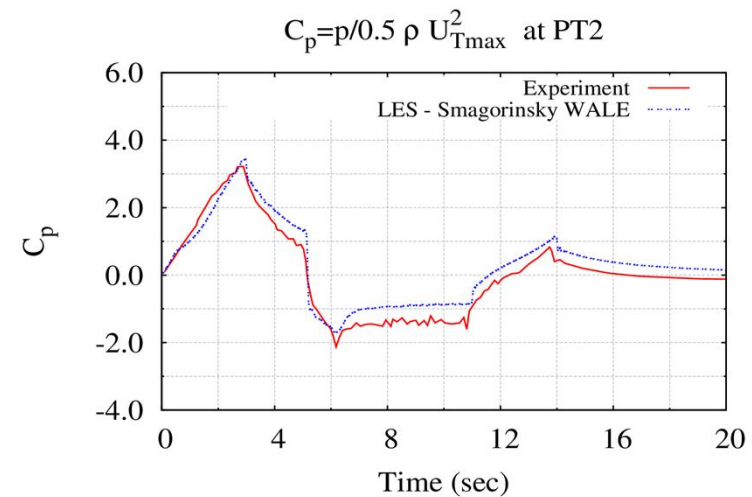
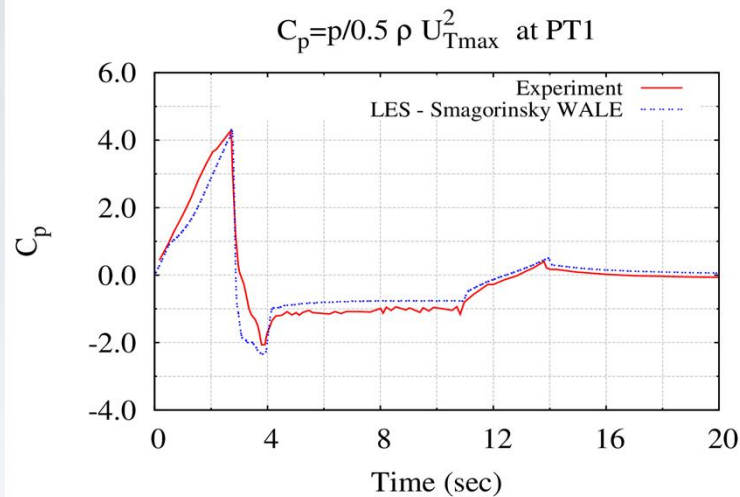
# Pressure Comparison



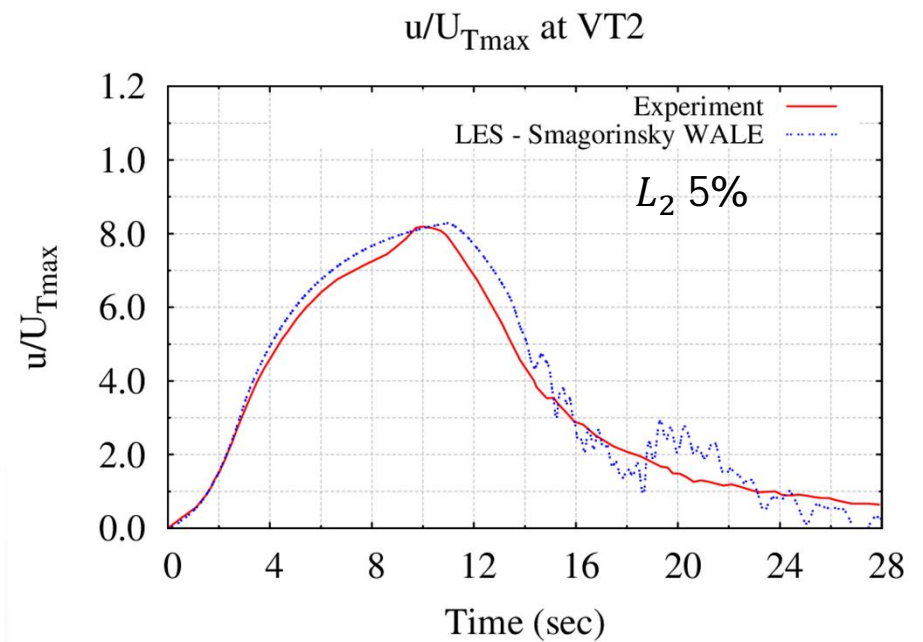
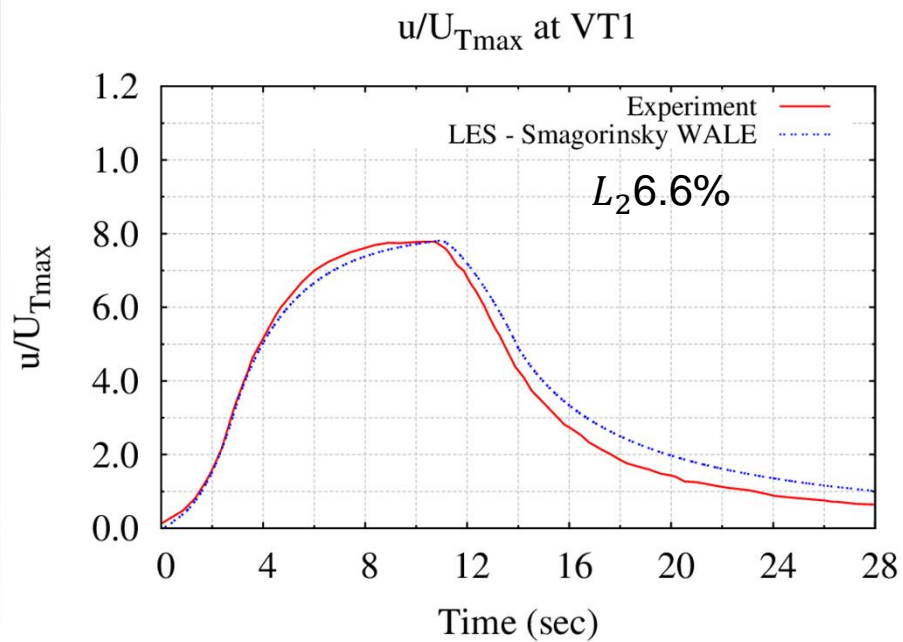
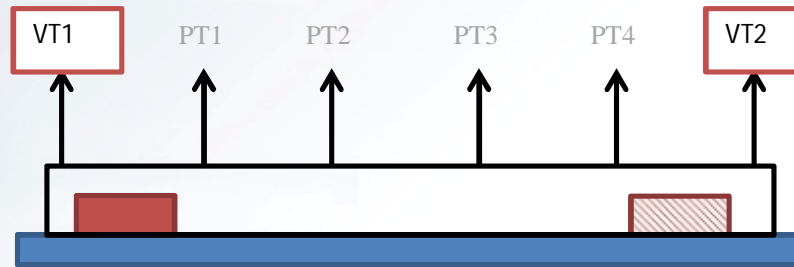


# Pressure Comparison

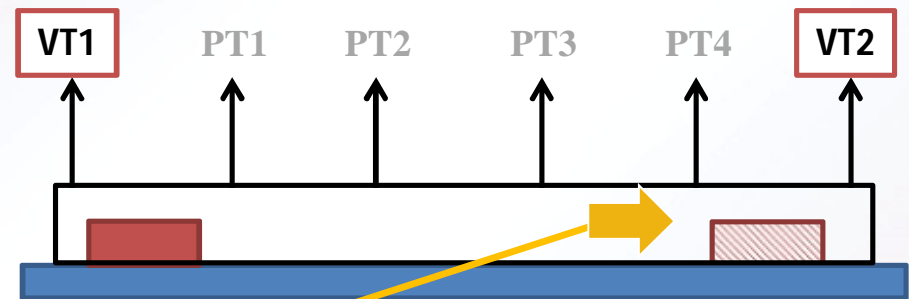
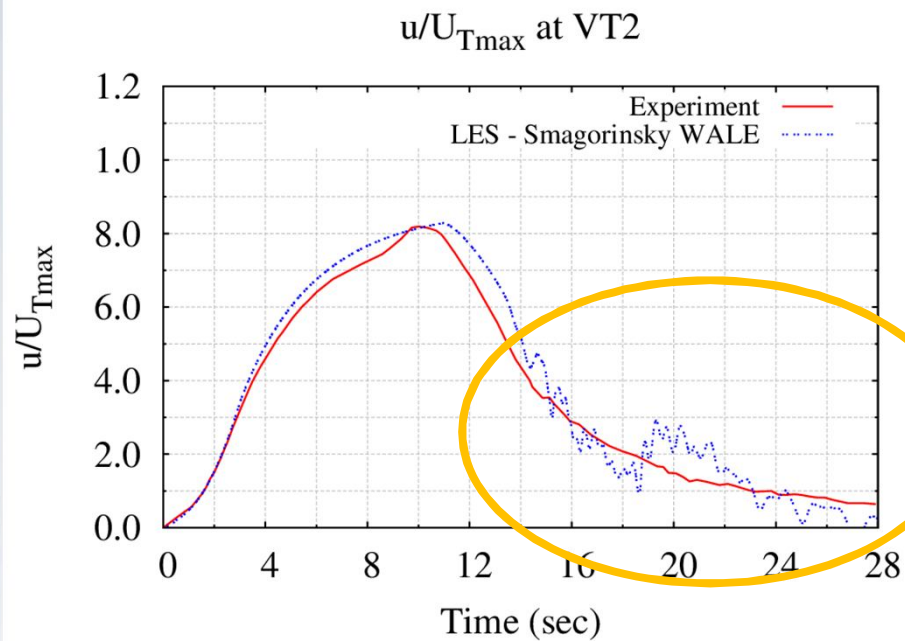
Refine the time step during the initial acceleration of moving body



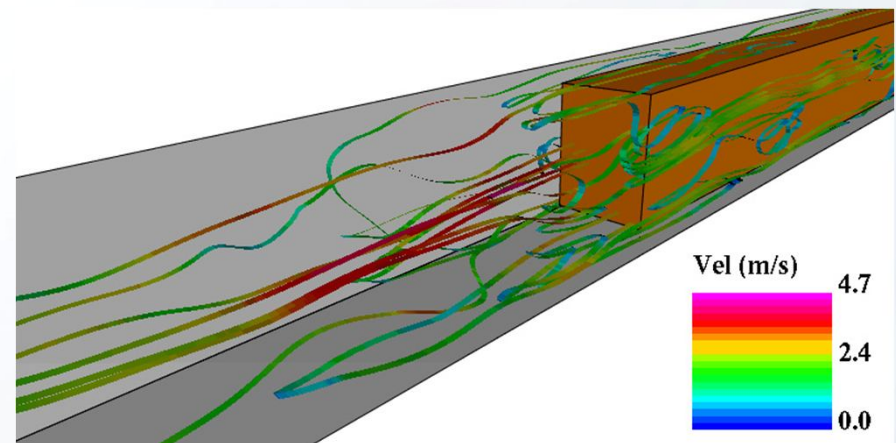
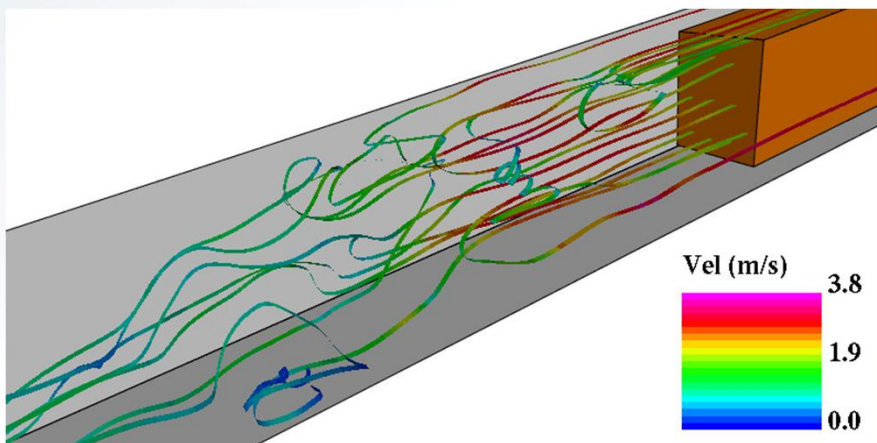
# Velocity Comparison



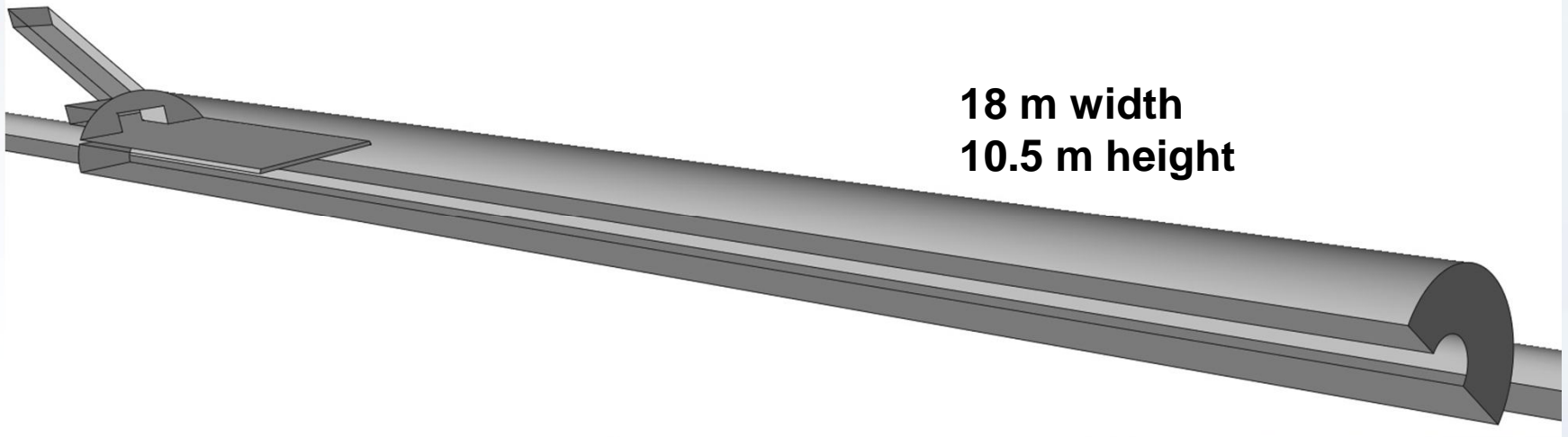
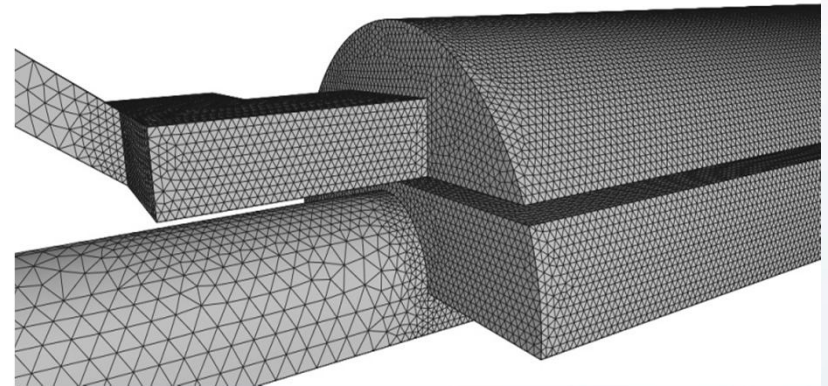
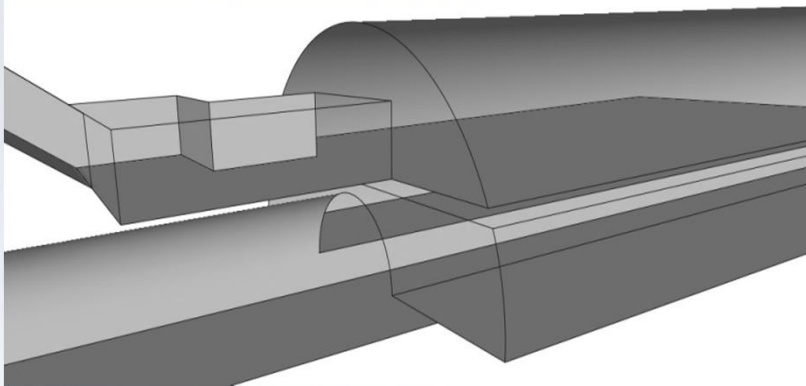
# Velocity Comparison



**High frequency velocity fluctuations due to wake blowback after the train comes to a stop.**



# Two Subway Stations





# Conditions

- Single subway car
- Speed 50 km/h
- Ambient temperature 20°C
- Temperature of subway base 50°C

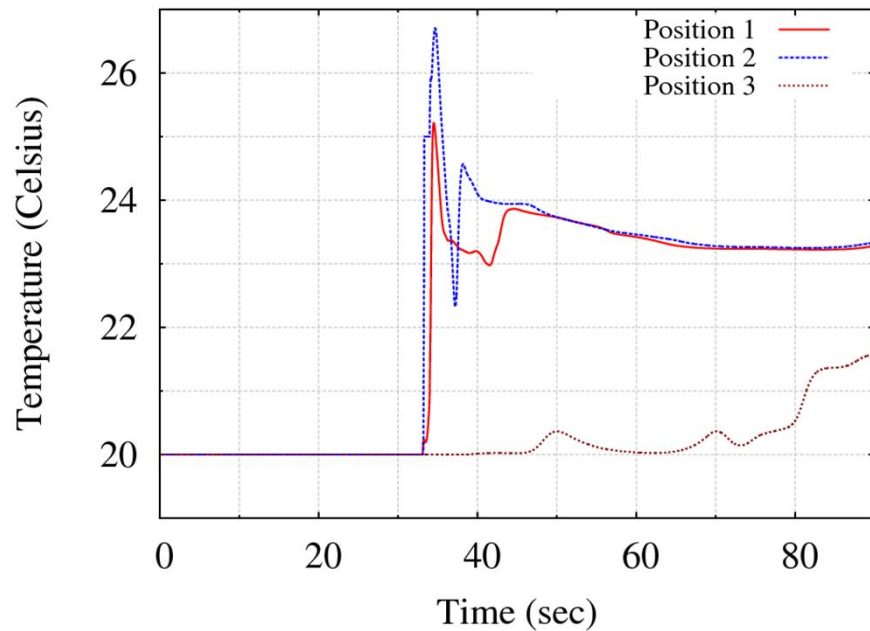
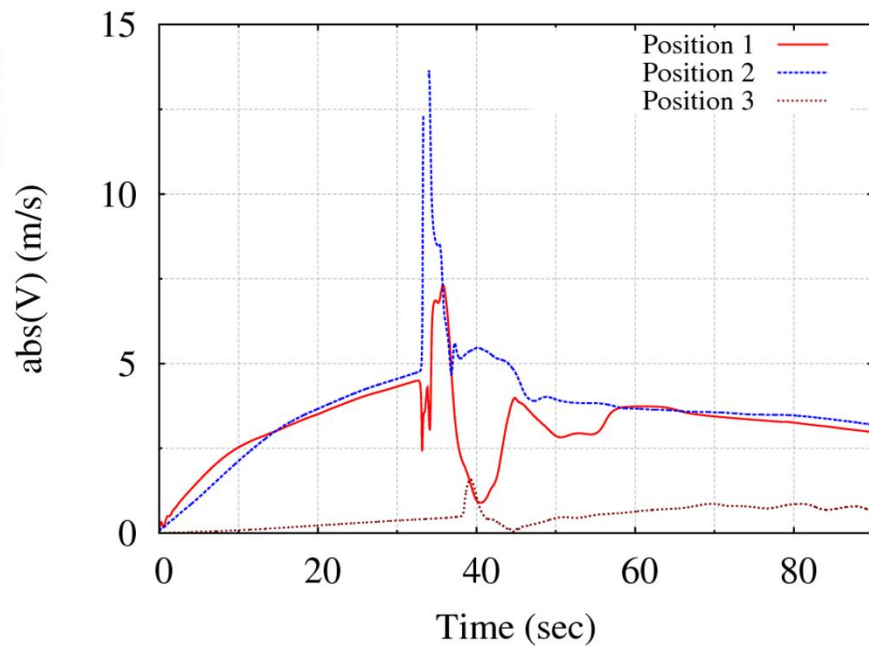
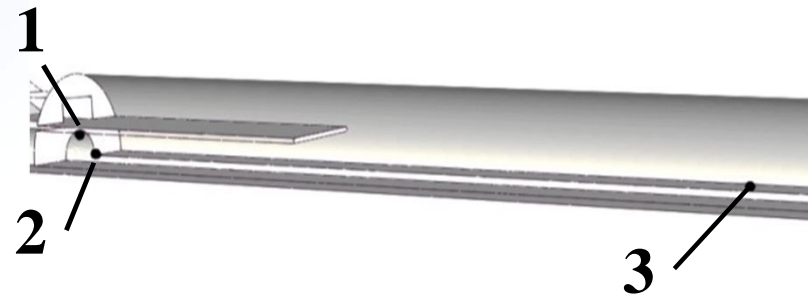
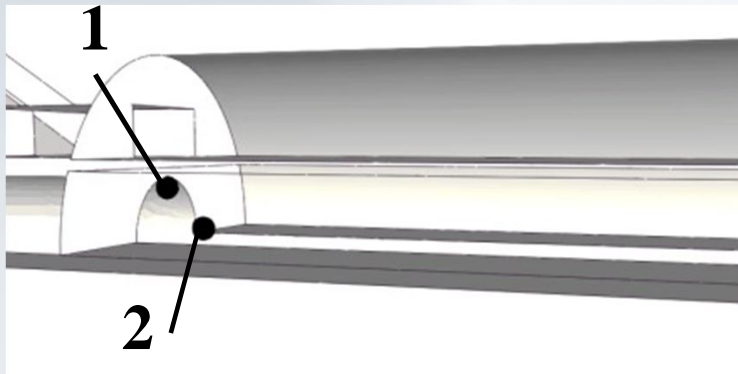
# Governing Equations

Continuity  $\nabla \cdot \vec{u} = 0$

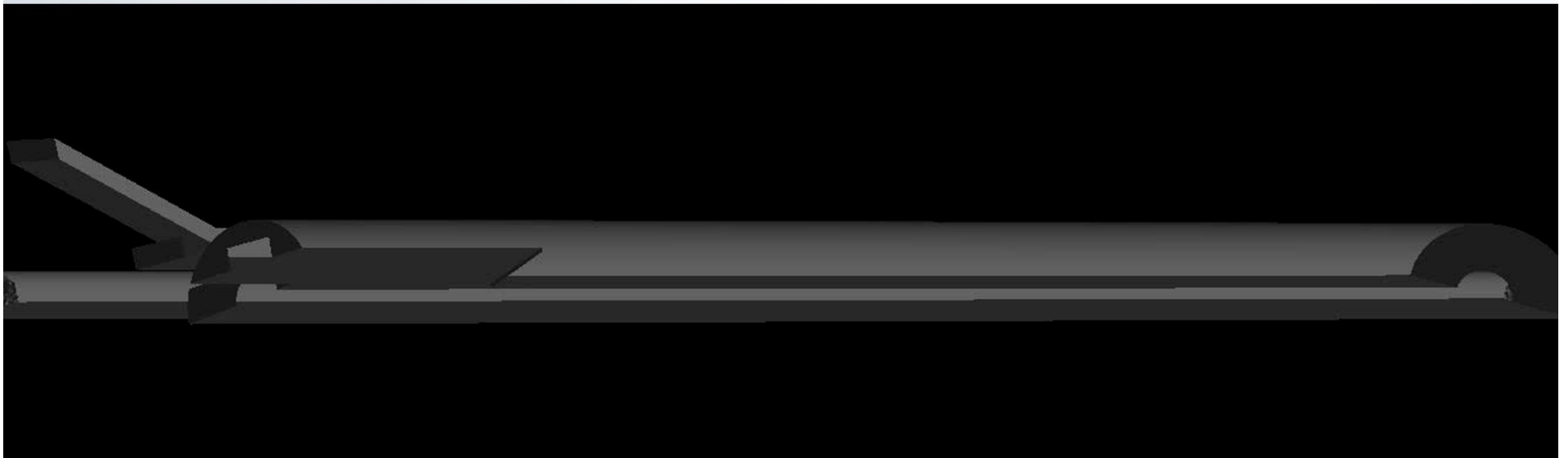
Navier-Stokes  $\rho \frac{D\vec{u}}{Dt} = \rho \vec{f}_e + \rho \vec{g}[1 - \beta(T - T_0)] - \nabla p + \mu \nabla^2 \vec{u}$

Temperature  $\rho c_p \left[ \frac{\partial T}{\partial t} + \vec{u} \cdot \nabla T \right] = \nabla \cdot (\kappa \nabla T)$

# Velocity and Temperature in Station 2

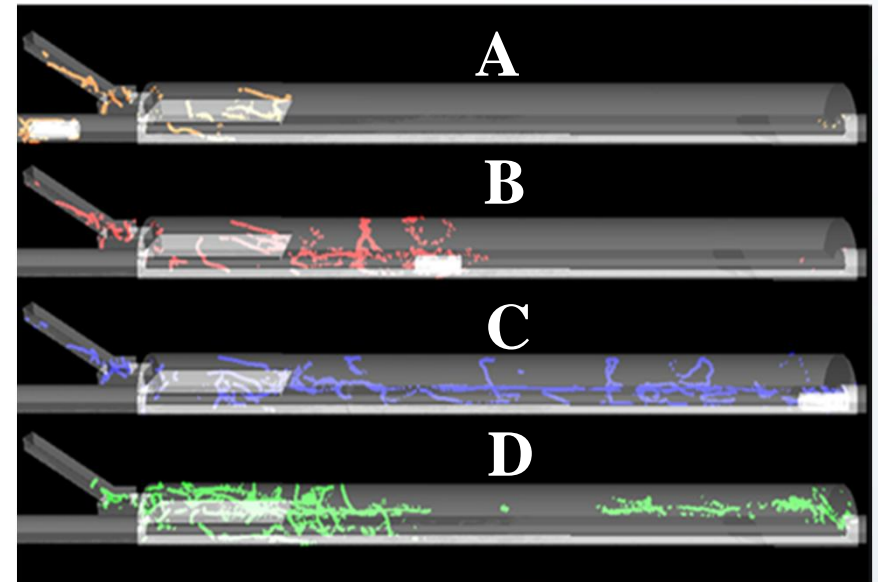
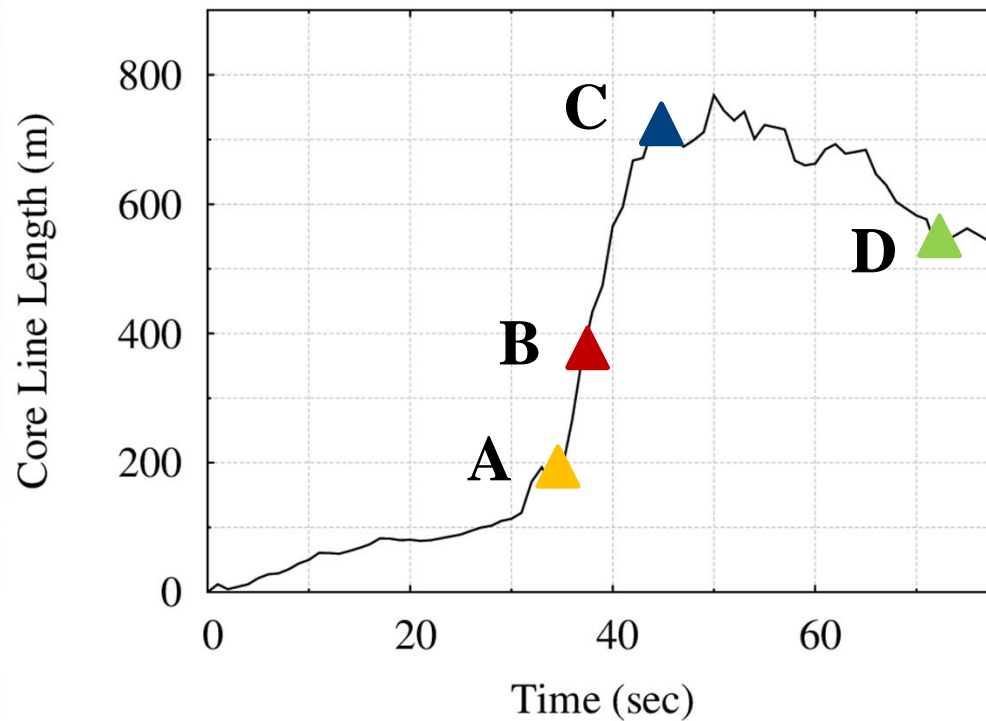


# Vortex Core Lines in Station 2

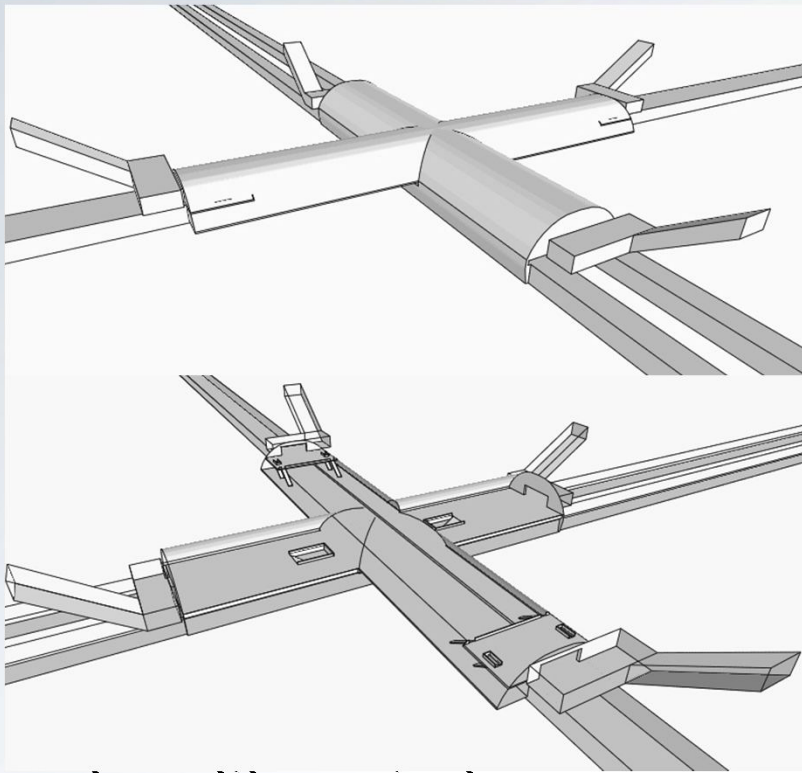




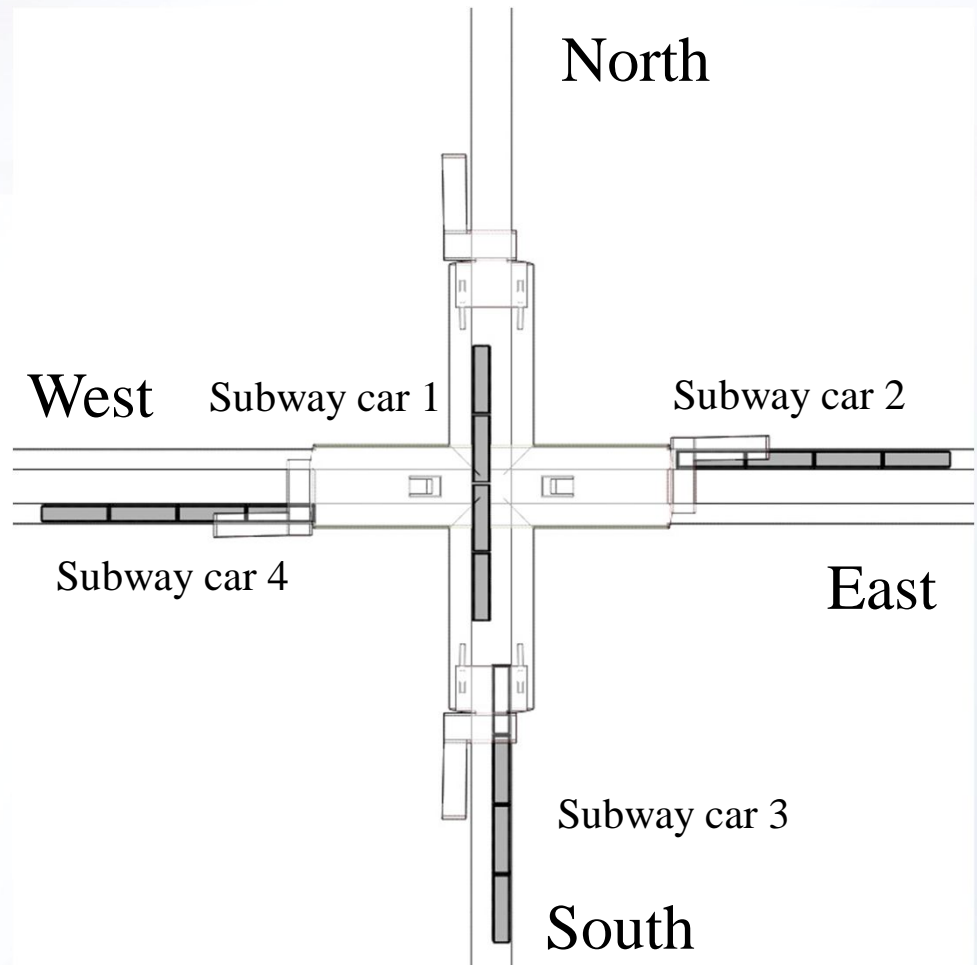
# Spatial Flow Complexity in Station 2



# Two-level Subway Station (Metro Center)



- 4 multi-car trains
- Realistic scheduling
- Multi-platform levels
- Stairwells connections between levels and the street



# Conditions

- Ambient temperature  $20^{\circ}\text{C}$
- Temperature at bottom of subway  $50^{\circ}\text{C}$
- Temperature on subway walls  $25^{\circ}\text{C}$
- Initial wind speed in tunnels and station is zero

# Governing Equations

Continuity  $\nabla \cdot \vec{u} = 0$

Navier-Stokes  $\rho \frac{D\vec{u}}{Dt} = \rho \vec{f}_e + \rho \vec{g}[1 - \beta(T - T_0)] - \nabla p + \mu \nabla^2 \vec{u}$

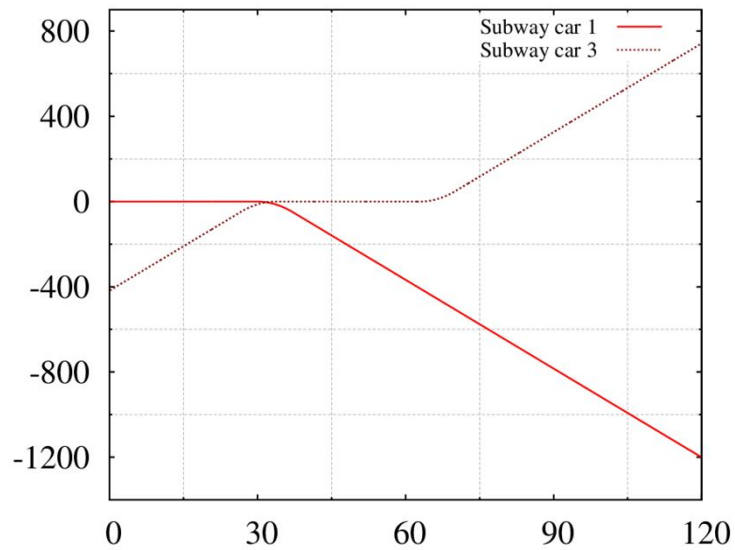
Temperature  $\rho c_p \left[ \frac{\partial T}{\partial t} + \vec{u} \cdot \nabla T \right] = \nabla \cdot (\kappa \nabla T)$

Concentration  $\frac{\partial c}{\partial t} + \vec{u} \cdot \nabla c = \nabla \cdot (D \nabla c) + S$

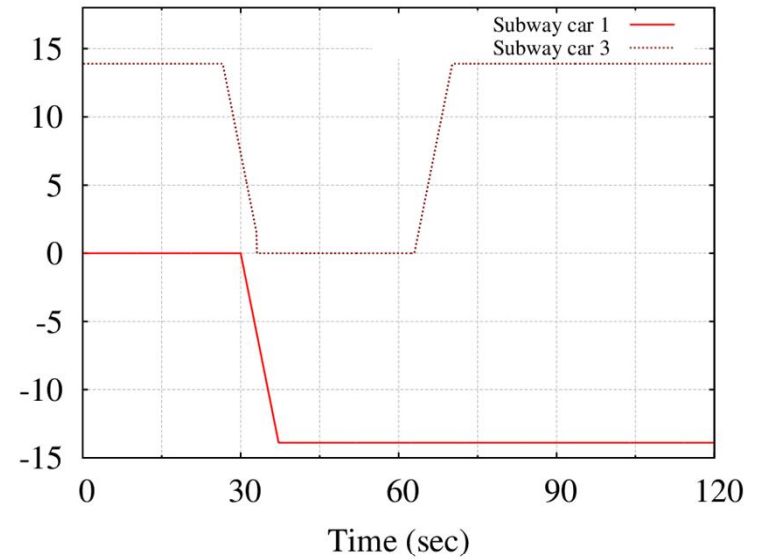


# Train Schedules

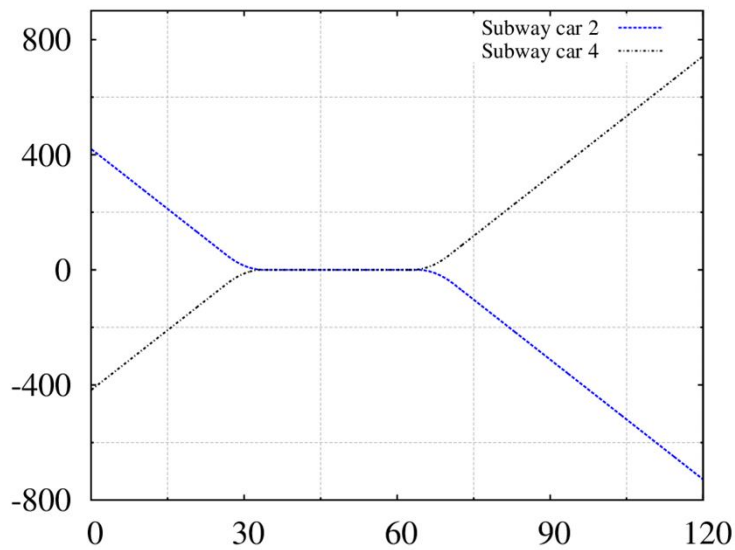
Position of North-South Subway cars (m)



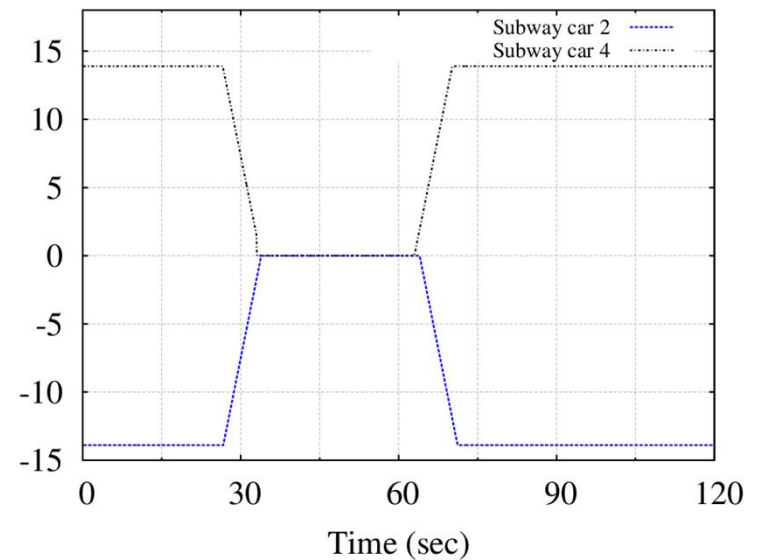
Speed of North-South Subway cars (m/s)



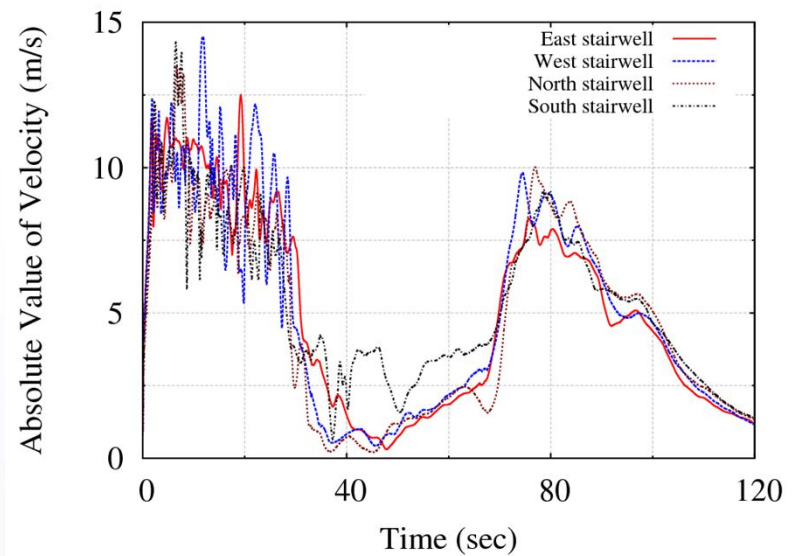
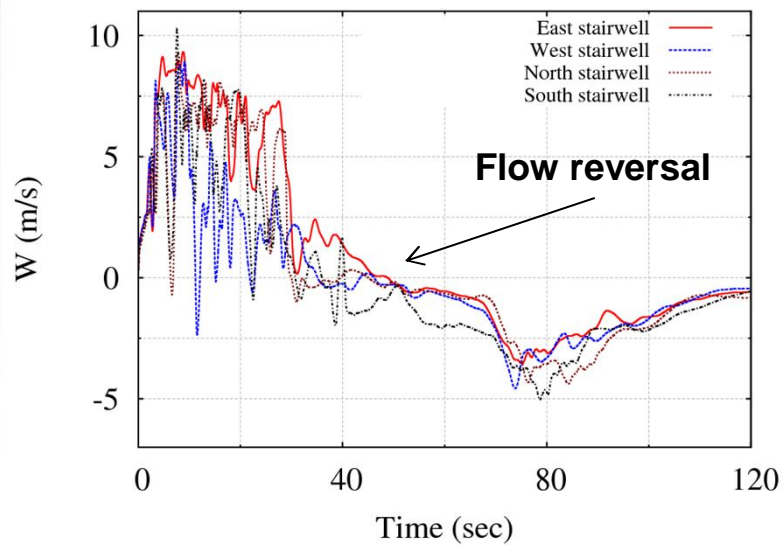
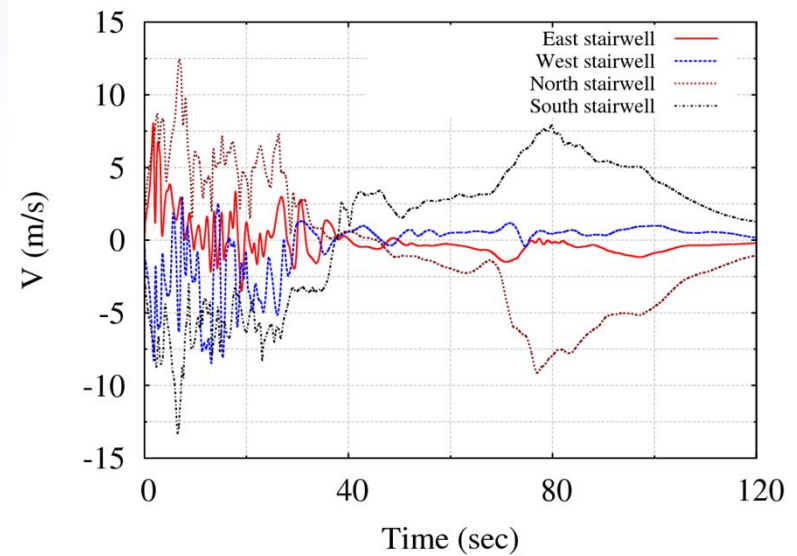
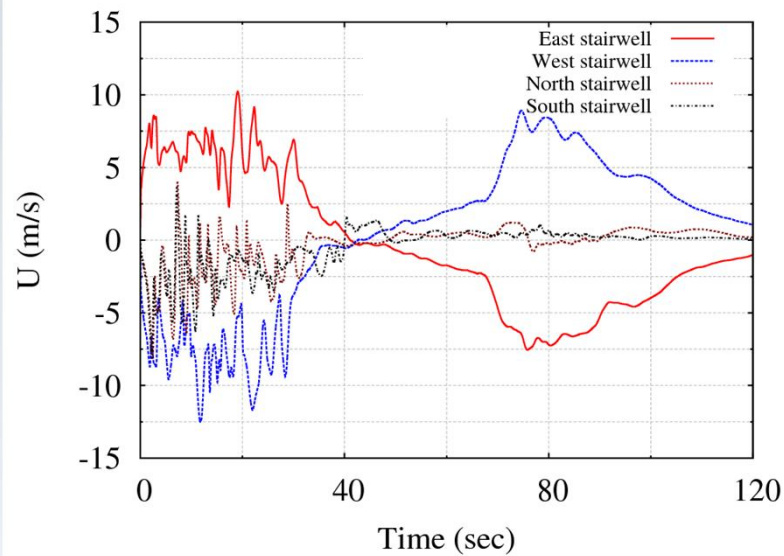
Position of West-East Subway cars (m)



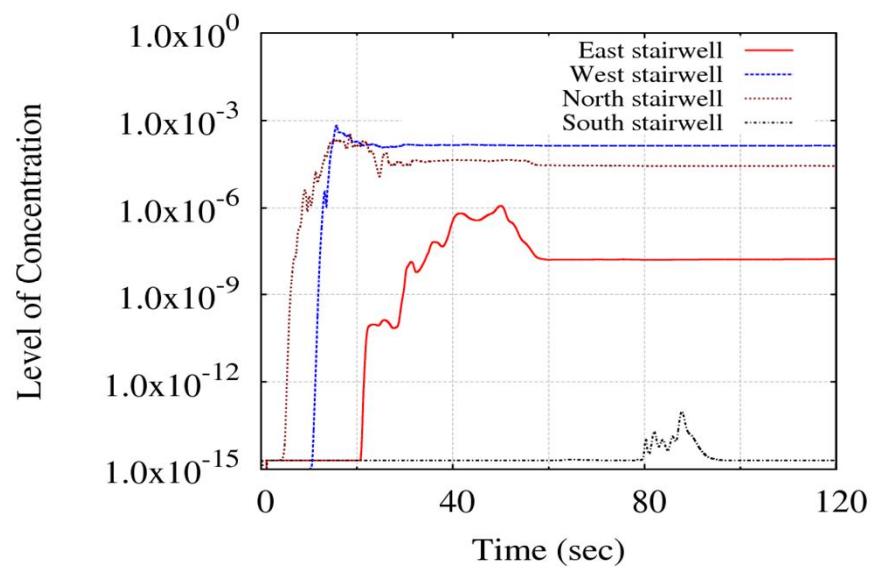
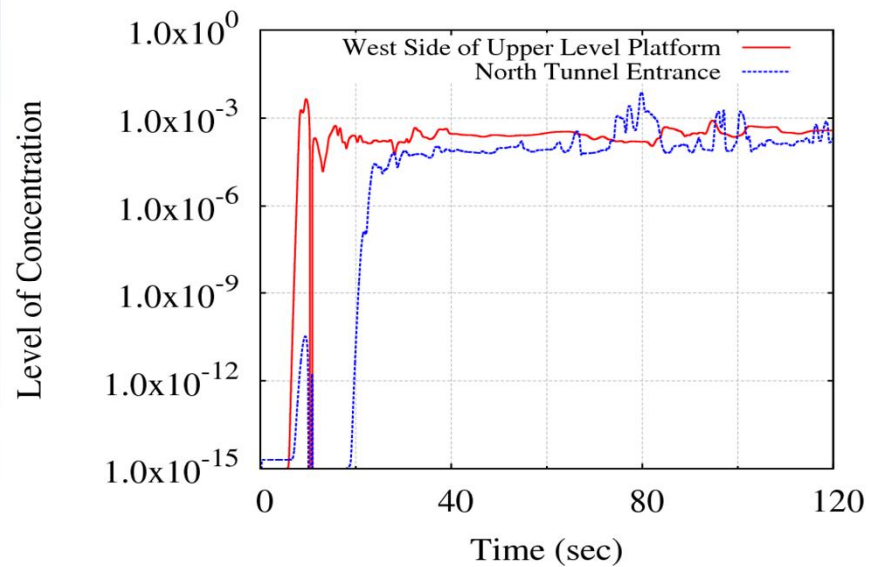
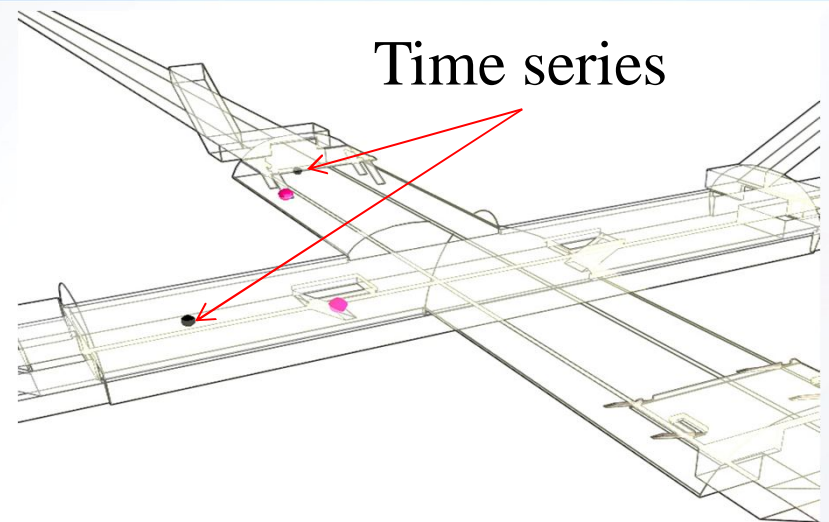
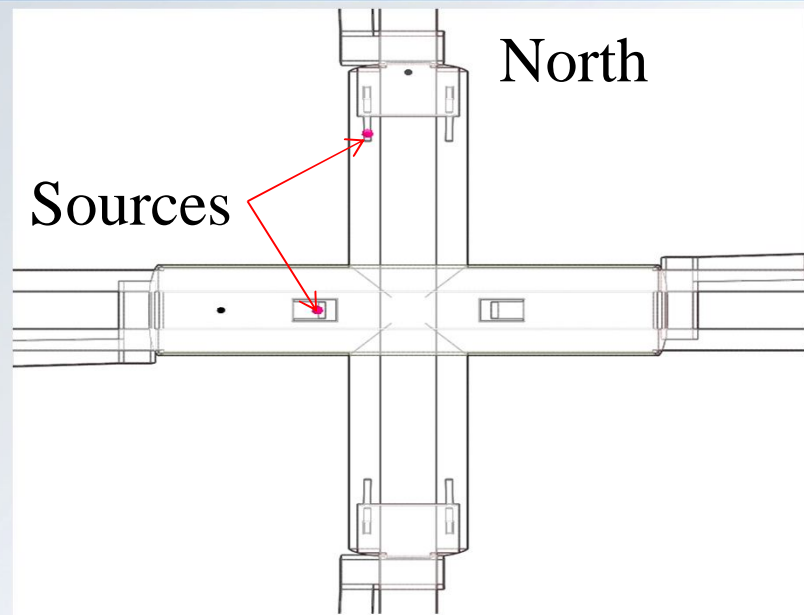
Speed of West-East Subway cars (m/s)



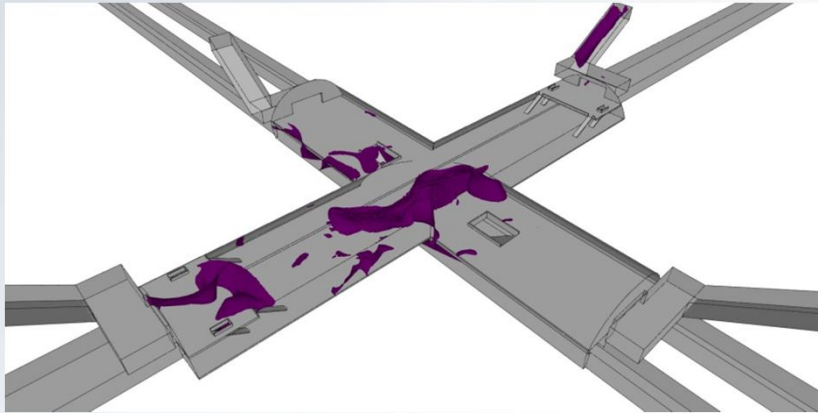
# Velocity Measurements



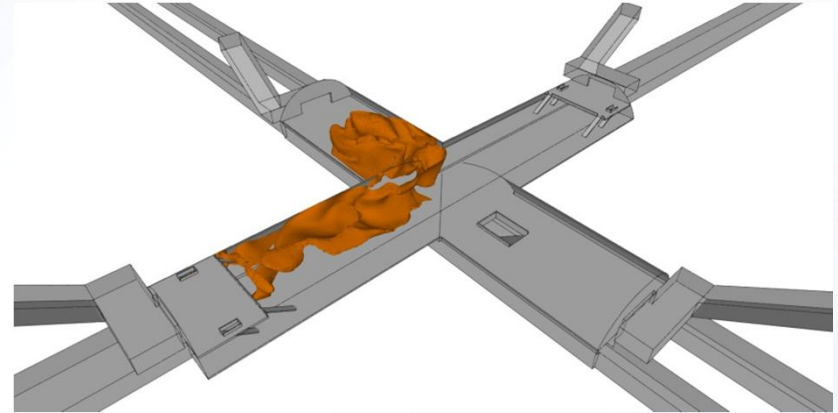
# Contaminant Release



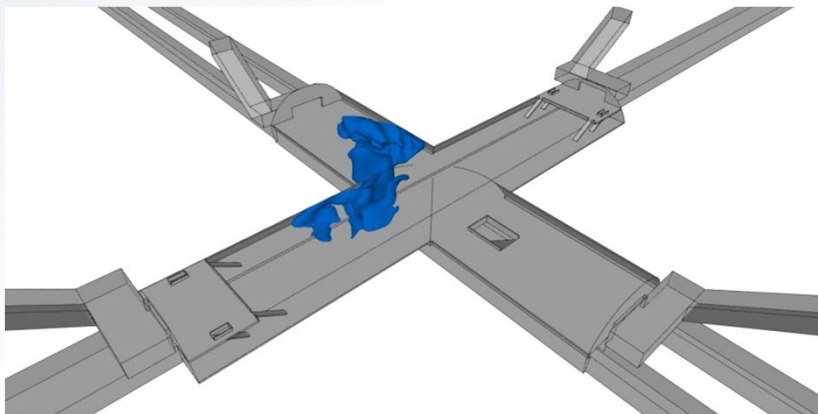
# Iso-surfaces 70 Seconds After Release



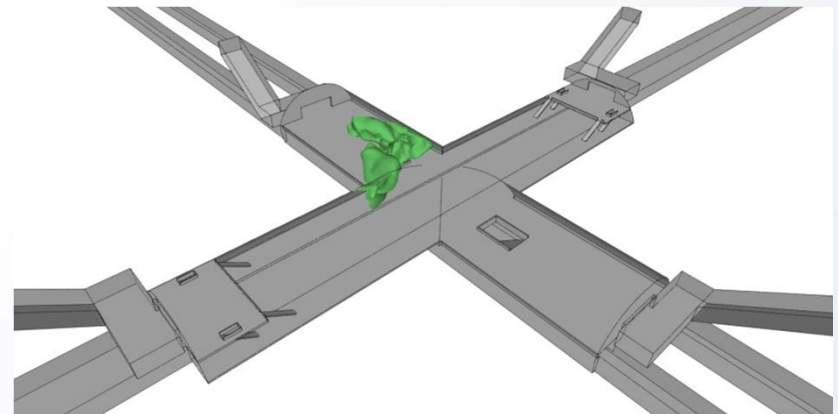
Concentration level of  $1.0 \times 10^{-5}$  ppm.



Concentration level of  $3.4 \times 10^{-4}$  ppm..

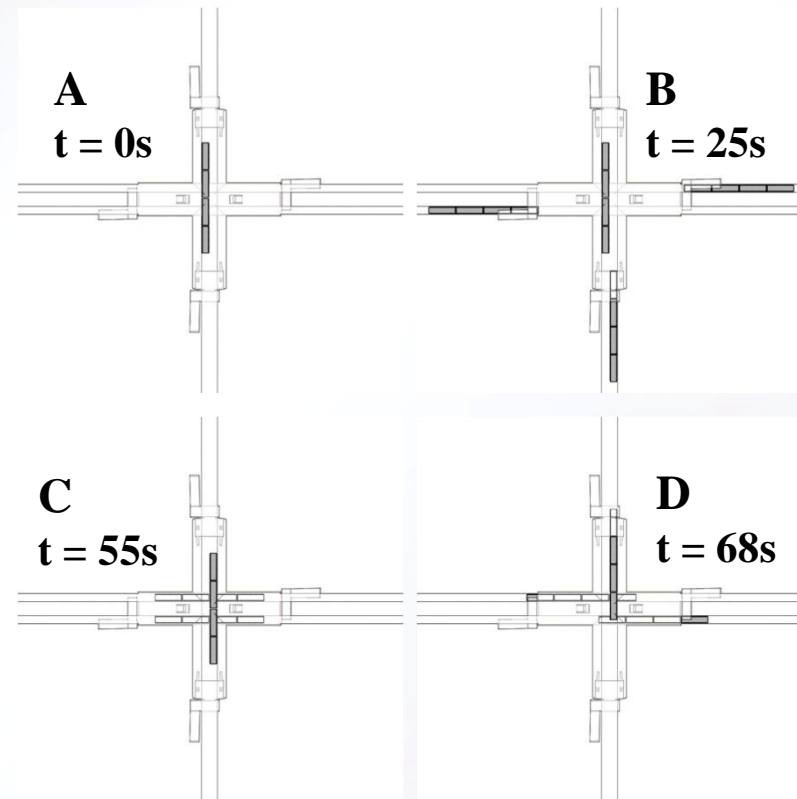
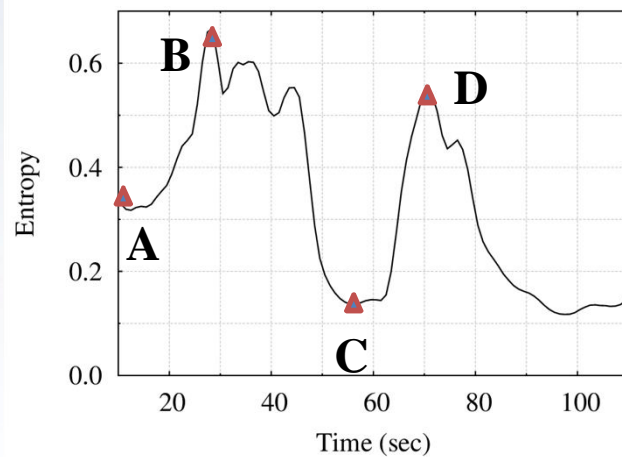
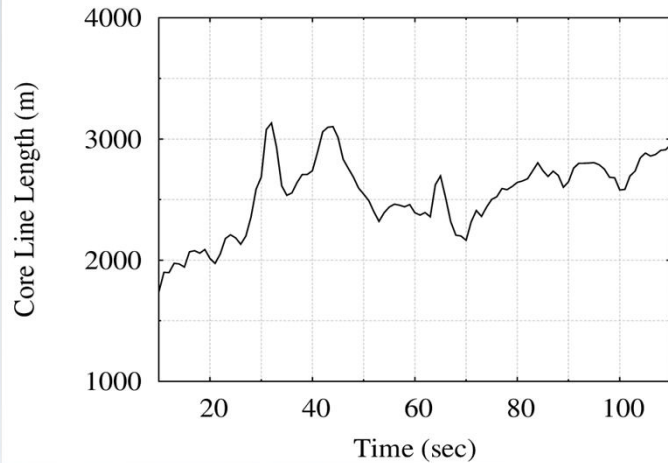


Concentration level of  $6.7 \times 10^{-4}$  ppm.



Concentration level of  $1.0 \times 10^{-3}$  ppm..

# Flow Characterization



- Spikes in the flow variables pinpoint complex spatiotemporal flow patterns.



# Conclusions

- We develop a more realistic CFD approach to model air flow in subway tunnels and stations.
- Simulations using the immersed body approach were validated against experimental data.
- The approach was extended for realistic station geometries, multi-car trains with schedules, street coupling and temperature profiles.
- Spatiotemporal flow structures were quantified within the station to study conditions leading to enhanced station contamination.

# Outlook

- Experimental data from a subway station in Dortmund, Germany. Unresolved B.C.
- In search of controlled experimental data (e.g. wind tunnel) for detailed comparisons.

